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#### 12 Abstract

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Full-waveform inversion (FWI) method has been proved as an effective tool for 13 high-resolution imaging of the subsurface. We have investigated the potential of 14 shallow seismic-wave 2D viscoelastic FWI as a method in high-resolution hy-15 drogeological near-surface characterization. FWI is applied to two orthogonal 16 profiles acquired at the Krauthausen natural laboratory (Germany). The multipa-17 rameter models of viscoelastic FWI (P-and S-wave velocities, attenuation of P-18 and S-waves, density) show pronounced lateral variations below the profiles. The 19 groundwater table is located at around 2 m, where a sudden P-wave velocity in-20 crease occurs. An S-wave low velocity layer exists at the depth of 4-6 m with 21 a high Poisson's ratio value close to 0.5, which corresponds to a saturated sand 22 layer know from previous studies. 23

A K-mean cluster analysis is used to correlate and integrate information con-

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tained in the inverted results. By considering the derived Poisson's ratio, P-wave, and S-wave velocities by FWI, we can convert the complex relationship between the multivariate data into a lithological meaningful zonation of the survey region. By comparing the lithological units in the alluvial aquifer with the cone penetration tests clusters, the face maps provide valuable information about the subsurface heterogeneity and connectivity. This experiment indicates that the multiparameter models derived by viscoelastic FWI contain usefull information for high resolution near-surface aquifer characterization.

24 Keywords: Aquifer characterization; Full-Waveform inversion; Rayleigh waves

#### 25 1. Introduction

A reliable investigation of the aquifer is needed for environmental engineer-26 ing tasks such as monitoring the groundwater flow and characterizing the contam-27 inated transport. However, an accurate hydrogeological characterization is still 28 challenging due to the typically heterogeneous unconsolidated gravel aquifer. Tra-29 ditionally, a high vertical resolution of aquifer parameters can be obtained based 30 on 1-D well data, e.g. core penetration test, tracer experiments. However, cost-31 efficiency and practical considerations lead to limited drilling numbers for 2D or 32 even 3D geometry. Sedimentary deposits are usually composed of several distinct 33 facies by recognizable boundaries at which the properties change (e.g. hydraulic 34 parameters and/or velocities) (Gueting et al., 2015). Thus, non-invasive methods 35 could help to characterize the geometry of the basement, classify the geophysi-36 cal or/and hydrological units or facies in 2D and 3D versions. High-resolution 37

<sup>38</sup> 2-D or 3-D geophysical (mostly electromagnetic and electrical) methods have
<sup>39</sup> been increasingly used to investigate heterogeneous aquifer (Mouhri et al., 2013;
<sup>40</sup> Klotzsche et al., 2013; Gueting et al., 2015, 2017; Yu et al., 2021, 2022).

Seismic refraction methods have also been used to carry out hydrogeological 41 investigations such as delineating groundwater aquifer in the subsurface (Jarvis 42 and Knight, 2002; Bradford and John, 2002; Bradford and Sawyer, 2002; Murad 43 et al., 2013). P-wave velocity  $(V_P)$  from seismic refraction methods can be used 44 to determine the water table depth. Furthermore, seismic cross-well tomography 45 (Moret et al., 2006; Becht et al., 2007) are performed for high-resolution aquifer 46 characterization. However, P-wave velocities will be affected not only by fluid 47 saturation, but also mineral composition, temperature, mineral texture, and other 48 effects (Bauer et al., 2003). Due to the ambiguity of  $V_P$  values, joint studies of  $V_P$ 49 and  $V_S$  can offer a suitable evaluation of aquifer characterization (Pasquet et al., 50 2015; Azhar et al., 2019). Besides, multichannel analysis of surface waves method 51 (Xia et al., 1999) is included to verify S-wave velocities and interpretations from 52 seismic refraction results (Konstantaki et al., 2013; Fabien-Ouellet and Fortier, 53 2014; Pasquet et al., 2015; Azhar et al., 2019). 54

In shallow seismic data, large velocity contrasts often generate wavefields with dominant higher modes of surface waves (Boaga et al., 2013; Gao et al., 2014, 2016). In this case, current surface-wave methods face uncertainty in the correct estimation and identification of multi-modal dispersion curves. Besides, the previous analysis of the ratio by the body waves commonly requires conducting two separate acquisitions for both  $V_P$  and  $V_S$ . As an alternative to conducting separate

acquisition surveys, full waveform inversion (FWI) may cope with these limita-61 tions and can derive high-resolution multi-parameter models for complex geo-62 logical structures simultaneously. With the rapid development of computational 63 power, it has become increasingly popular to use 2D FWI of surface wave for 64 reconstruction of near-surface models (Romdhane et al., 2011; Tran et al., 2013; 65 Groos et al., 2014, 2017; Pan et al., 2016, 2019; Pan and Gao, 2020; Dokter et al., 66 2017). However, most of the previous studies invert for S-wave velocity only and 67 neglect the effects of attenuation or simply implement a passive-viscoelastic FWI 68 approach in which a fixed prior estimation of the attenuation model is used in 69 the forward modeling to compensate for viscoelastic effects. When facing strong 70 spatial variation of strong attenuation in shallow subsurface where a high level 71 of heterogeneity exists, simply neglecting the viscoelastic effect might deterio-72 rate the reconstruction of S-wave velocity (Groos et al., 2014; Gao et al., 2020). 73 Multi-parameter full waveform inversion could reconstruct both velocity and at-74 tenuation simultaneously (Métivier et al., 2013; Yang et al., 2018; Fabien-Ouellet 75 et al., 2017; Athanasopoulos et al., 2020; Gao et al., 2021). Besides, 3D FWI of 76 the near-surface parameter reconstruction is also becoming feasible in the recent 77 years (Irnaka et al., 2019; Mirzanejad and Tran, 2019; Pan et al., 2021). 78

In this paper, we present a case study for aquifer characterization with 2D viscoelastic FWI. We conducted a field experiment at the Krauthausen test site in Northwest Germany, where seismic data were acquired along two orthogonal lines. Intensive cone penetration tests (CPT) have been conducted there, together with an intensive investigation of Ground Penetrating Radar (GPR) data. Due to

the extensive set of subsurface information retrieved, this test site offers an excel-84 lent opportunity to test the potential of seismic data for aquifer characterization. 85 The detailed subsurface geological information about the test site is provided in 86 Section 2. Firstly, the seismic FWI is applied to estimate both P- and S-wave ve-87 locity, attenuation of P and S waves, and thereby Poisson's ratio. The description 88 of the methodology is presented in Section 3. In Section 4, the outcome of the 89 inversion enables us to understand in detail the lateral variation in layer thickness 90 and properties. Later, a cross-sectional map showing the spatial distribution of 91 the subsurface presents the connectivity of the obtained two profiles. Secondly, a 92 K-mean cluster analysis is conducted for the facies classification by considering 93 their  $V_p$ ,  $V_s$ , and Poisson's ratio. The clustering result shows the spatial distri-94 bution of different facies in the aquifer. Finally, we discuss the reliability of the 95 facies classification by comparing the distribution of facies obtained from seismic 96 FWI to the cluster analysis results of the data from CPT. 97

#### 98 2. Field data application

#### 99 2.1. Description of the test site

The goal of seismic survey was to characterize the hydrological situation at the Krauthausen test site. It is located in northwest Germany between cities of Jülich and Düren and was set up in 1993 by research center Jülich. Over the last decades, the Krauthausen site has been intensively investigated with the goal of studying the spatial distribution of aquifer with a broad spectrum of methods, including tracer experiments (Vereecken et al., 2000), cone penetration tests (Tillmann et al.,

2008), and geophysical imaging methods (Klotzsche et al., 2013; Gueting et al., 106 2015, 2017). The present studies showed that the uppermost aquifer is approxi-107 mately 10 m thick and composed of alluvial terrace sediments (Fig. 1). The top of 108 the aquifer was divided into three layers: a poorly-sorted gravel layer extending 109 from 1-4 m depth; a well-sorted sand layer extending from 4-6 m depth; and a 110 bottom layer composed of sandy to gravel grain size, which extends from 6-11.5 111 m depth. The groundwater level shows variations from 1 to 3 m depth depending 112 on the annual season. It is worth to note the generalized aquifer shown in Fig.1 113 represents a conceptual model of the geologic sequence for the aquifer, which is 114 an oversimplification of the aquifer's true structure. 115

Most recently GPR full-waveform inversion revealed the heterogeneous nature 116 of the uppermost aquifer with higher spatial resolution and yielded a tomographic 117 image with a significantly improved level of details (Klotzsche et al., 2013; Guet-118 ing et al., 2015, 2017). Besides, CPT were performed in the centre of the test site 119 with a vertical sampling interval for all measurement set as 10 cm. At each CPT 120 location, vertical profiles are down to an average depth of approximately to 13 m 121 (Gueting et al., 2015), which could across the entire thickness of the uppermost 122 aquifer. 123

#### 124 2.2. Data acquisition

With the aim of delineating the lateral variation of the subsurface in the Krauthausen test site, the seismic surveys were conducted along two perpendicular lines. The acquisition was implemented on the 29th and 30th of September 2018 under rela-



Figure 1: Left: Schematic diagram map of the Krauthausen test site including the two seismic profiles and adjacent boreholes and CPT positions. The asterisk and the dark dots represent the location of boreholes and the cone penetration tests, respectively. Right: A conceptual geologic cross-section of the uppermost aquifer in Krauthausen test site according to Döring (1997) and Tillmann et al. (2008).

tively dry soil conditions (Athanasopoulos, 2021). Two survey lines (P1 and P2) 128 were set in the central part of the test site, where closely spaced boreholes and 129 CPTs were available. The acquisition geometry of P1 consisted of 14 shots as 130 vertical-force sources with a spacing of 4 m and 48 receivers with a spacing of 1 131 m. The acquisition geometry of P2 consisted of 11 shots generated by vertical-132 force sources with a spacing of 4 m and 36 receivers with a spacing of 1 m. The 133 sources were generated by hammer blows hitting a steel plate. P1 crossed the 134 boreholes 67, 31/62, 26/61,22, 64, and 65, with the last one being the end of the 135 receiver line (Athanasopoulos, 2021). P2 was placed near the boreholes 48, 32, 136 38, 31, 62, and 30. A detailed map of the Krauthausen test site with two profiles 137 is shown in Fig. 1. 138

#### 139 3. Methodology

FWI, as a data-fitting iterative procedure, aims to minimize the differences between the simulated data and the measured data here defined as,

$$J(\boldsymbol{m}) = \frac{1}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \|\boldsymbol{d}_{cal}(\boldsymbol{m})(\boldsymbol{x}_r, t; \boldsymbol{x}_s) - \boldsymbol{d}_{obs}(\boldsymbol{x}_r, t; \boldsymbol{x}_s)\|^2.$$
(1)

Here, the model properties (such as velocity, attenuation, density) of the subsurface are denoted by the vector  $\boldsymbol{m}$ . Further,  $\boldsymbol{d}_{obs}$  and  $\boldsymbol{d}_{cal}$  represent the observed and synthetic seismograms computed in the model  $\boldsymbol{m}$ , associated with the source  $\boldsymbol{x}_s$  and receiver  $\boldsymbol{x}_r$ , respectively.  $N_s$  and  $N_r$  represent the source and receiver numbers, respectively. And t is the time. The inversion is formulated as the minimization of the misfit function J. To the large size of the model space, the global optimization method is computationally expensive for solving problems Xing and Mazzotti (2019). Hence, FWI is usually performed through the iterative local optimization technique based on gradients which can be calculated efficiently by the adjoint state method. In the framework of local non-linear optimization methods, an iterative sequence  $m_{k+1}$ is built by starting from an initial guess  $m_0$  with a descent direction  $\Delta m_k$ :

$$\boldsymbol{m}_{k+1} = \boldsymbol{m}_k + \lambda \Delta \boldsymbol{m}_k \tag{2}$$

where k is the iteration number, and  $\lambda$  is the step length at iteration k estimated through a line search process with parabolic fitting (Nocedal and Wright, 2006). The model perturbation,  $\Delta m_k$ , can be given by gradient-based (e.g. steepest descent, conjugate gradient) and Newton-based method (e.g. truncated Newton method, Gauss-Newton method).

Multi-parameter FWI is challenging due to the potentially strong interparame-159 ter crosstalks (Virieux and Operto, 2009; Operto et al., 2013). Updating the model 160 perturbation with gradient only cannot decipher between different parameters. Re-161 searches show that Newton-based methods generate less crosstalk and artefacts in 162 the reconstructed models (Métivier et al., 2013; Yang et al., 2018; Gao et al., 163 2021). In this case, we implement the multi-parameter viscoelastic FWI with the 164 matrix-free Gauss-Newton algorithm. The general scheme for solving the multi-165 parameter includes two loops: an external loop for Gauss-Newton update and the 166

inner loop is the linear conjugate gradient method. For a more detailed description
tion of the inversion procedure and its implementation, the reader could refer to
Bohlen et al. (2021) and Chen and Sacchi (2020).

An important requirement for the full-waveform inversion is adequate starting 170 models (Pan et al., 2019). To derive adequate  $V_S$  starting models, we conducted 171 the Multi-channel analysis of Surface wave (MASW) method for profile P1 (Xia 172 et al. (1999)). The initial 1D  $V_P$  model is calculated from the first-arrival times 173 of the refracted waves. The initial  $\rho$  models are obtained through Gardner's rela-174 tionship. For the initial  $Q_P$ ,  $Q_P = 2 * Q_S$  is assumed. Linear gradient models are 175 used as the initial models for inversion. All five initial models are shown in the 176 first column of Fig. 2. Before the inversion, a 3D to 2D transformation (Forbriger 177 et al., 2014) must be applied to the field data. Schäfer et al. (2014) proved the 178 applicability of this 3D to 2D transformation even to models with smooth lateral 179 heterogeneities. To reduce the non-linearity of the inverse problem and avoid the 180 inversion being trapped into a local minimum, a sequential FWI workflow of low-181 pass and band-pass filtered data with different bandwidth is applied (Bunks et al., 182 1995). In our example the multi-stage inversion strategy with the frequency band 183 starts with low-pass filter data with 0 - 15 Hz. The frequency content is progres-184 sively increased by 5 Hz until 40 Hz is reached, and a highest frequency band of 185 60 Hz is used in the last stage. 186

#### 187 4. Results

In this section, we present the inverted model obtained from multiparameter viscoelastic FWI. A minimum of three iterations is guaranteed in each stage, and the inversion moved to the next stage when the relative decrease in the misfit value is less than 1%. We estimate a source time function correction filter by a stabilized deconvolution (Groos et al., 2014) and use it to update the source time function at the beginning of each frequency stage.

The multi-parameter inversion results along both profiles are shown in Fig. 194 2. The reconstructed  $V_S$  structure shows a high level of heterogeneity. Below 195 the P1 profile,  $V_S$  is low within the upper 2 m where the loamy soil layer has 196 developed (Döring, 1997; Gueting et al., 2015). Referring to the prior geological 197 model (Fig. 1) of the test site (Tillmann et al., 2008), there is a poorly sorted 198 gravel layer that exists in the depth of about 2 - 4 m, where the  $V_S$  increases. A 199 layer of low  $V_S$  shows up at the depths of 4 - 6 m, which correlates well with 200 previous studies that a sandy layer exists. Especially, the P2 profile shows a more 201 continuous and distinct boundary of this sand layer, which can also be comfirmed 202 in Athanasopoulos (2021). Below this layer,  $V_S$  increases, which agrees to the 203 borehole information that the soil content change from sand to gravel. Overall, the 204 S-velocity model is distinguished by sub-horizontal structures, which is consistent 205 with stratigraphic layering in the gravel and sand deposits at the Krauthausen test 206 site. 207

For  $V_P$  results from both P1 and P2 profiles, both of them did not show strong horizontal heterogeneity compared to  $V_S$  results. This low resolution can be at-



Figure 2: Final models below both profiles obtained by 2D viscoelastic FWI. The initial models are represented in the first column. The second column and third column represent the reconstruction results of profiles 1 and 2, respectively. Since we only use one relaxation mechanism (Bohlen, 2002; Gao et al., 2021),  $\tau_s$  and  $\tau_p$  are approximated as  $2/Q_s$  and  $2/Q_p$  where  $Q_s$  and  $Q_p$  are the quality factor of S and P wave, respectively.

tributed to the large wavelength of the P-wave at low frequencies. Nevertheless, consistent structures in the  $V_P$  results can be observed. We can see the P-wave velocity is suddenly increased at the depth of about 2 m, where the groundwater table exists. It is confirmed that the effect of water saturation on  $V_P$  is significant. This sudden increase could thus be an indicator of groundwater table level in the near-surface cases (Pasquet et al., 2015).

The inverted attenuation models of both profiles are given in Fig. 2. We 216 inverted for the so-called tau parameter which relates to the quality factors of P-217 and S-waves by  $Q_s \approx 2/\tau_s$  and  $Q_p \approx 2/\tau_p$ . For the  $\tau_s$  results, we can observe clear 218 strong attenuation anomalies located at the depth of 4-6 m. For the  $\tau_p$  results, as 219 can be seen that the results are significantly contaminated by some artefacts. This 220 could be interpreted as attenuation is the weakest parameter and can be easily 221 affected by velocity and density errors (Fabien-Ouellet et al., 2017; Gao et al., 222 2020, 2021). As to the inverted density model (Fig. 2) in P1, the reconstructed 223 results did not provide reliable information about the surface layers. With regards 224 to the density model in P2, it delineates a high-density layer at about 3-5 m. Due 225 to the low sensitivity of the Rayleigh wave to density, the reliability of the density 226 results needed to be the verified by some secondary data. 227

#### 228 4.1. Poisson's ratio

Experimental developments (Bachrach et al., 2000; Foti et al., 2002; Uyanik, 2011) showed that the saturation could affect the P- and S-wave velocities ( $V_p$  and  $V_s$ ). This gives a hint that the joint studies of  $V_P$  and  $V_S$ , especially by estimating Poisson's ratio could provide a suitable evaluation of the saturation of aquifer
characterization (Bachrach et al., 2000; Konstantaki et al., 2013; Pasquet et al.,
2015).

Using the inverted  $V_P$  and  $V_S$ , we also calculate the Poisson's ratio as

$$\nu = \frac{V_P^2 - 2V_S^2}{2(V_P^2 - V_S^2)}.$$
(3)

The computed  $\nu$  results obtained by  $V_P$  and  $V_S$  in Fig.2 are remarkably similar 236 (Fig. 3f). As can be seen in the initial Poisson's ratio model, the initial value of 237 Poisson's value is 0.42. While the Poisson's ratio values of the reconstructed 238 results for both profiles range from 0.3 to 0.5 (second and third column in Fig. 239 2), which are typical of unsaturated and saturated media, respectively (Pasquet 240 et al., 2015, 2016). Lower Poisson's ratio values at the shallow subsurface may 241 be explained by the dry soil condition on the top layer (Athanasopoulos, 2021). 242 Specifically, the Poisson's ratio closes to 0.5 at the depth of 4-6 m, might indicate a 243 highly saturated layer located there, and corresponds to existed sandy layer. This 244 result also shows a good agreement in both profiles together with the previous 245 study (Döring, 1997; Gueting et al., 2015). 246

<sup>247</sup> We show the results of all inverted parameters from both profiles into a 3D <sup>248</sup> layout (Fig. 3). The cross-sections show a good agreement in the majority of <sup>249</sup> the results. The low S-wave velocity layer with a high Poisson's ratio delineates <sup>250</sup> the high saturated sandy layer at the depth of 4-6 m. The sudden increase in  $V_P$ <sup>251</sup> indicates the location of the water level. To further evaluate the inverted results,



Figure 3: Cross-section of the reconstructed models of both profiles by multi-parameter FWI. (a)  $V_S$ ; (b)  $V_P$ ; (c)  $\tau_s$ ; (d)  $\tau_p$ ; (e)  $\rho$ ; (f) Poisson's ratio. The red dots and blue triangles represent the shots and receivers, respectively.



Figure 4: (a) and (b) represent data misfit for P1 and P2, respectively; Jumps of increasing misfit value correspond to changes of the FWI workflow stage. (c) and (d) represent the comparison of the trace-normalized observed (black) and synthetic seismograms (red) for shot 5 in P1 and P2, respectively. The shot gather for the shot 5 in profiles 1 is displayed with every two traces. (e) and (f) represent the estimated source time functions of data acquire along P1 and P2, respectively.

the final data misfits are shown in Figs. 4a and b. We note that the data misfit 252 reduces. We also compare the final synthetic seismogram with the observed data 253 in Fig. 4e and f. In both profiles, the synthetic seismogram fits the observed data 254 in satisfactory, which indicates a successful explanation of the observed wavefield 255 by the final multi-parameter models. The final estimated source-time functions 256 (STF) for every shot in both profiles are shown in Fig. 4e and f. In both cases, 257 we can observe similar wavelets for all source locations, indicating that estimated 258 source time functions used for the inversion are fairly reliable. 259

#### 260 4.2. Cluster analysis

Cluster analysis, as a multivariate statistical method, can be used to correlate 261 and integrate information of a broad range of observations into relatively homoge-262 neous units by dividing the data based on their distances in the multi-dimensional 263 parameter spaces instead of a prior information about the classification. K-means 264 algorithm (Macqueen, 1967) has been proven as a useful approach to extract the 265 basic structural information from various types of multivariate geophysical data 266 (Tronicke et al., 2004; Dietrich and Tronicke, 2009). Shallow-seismic wavefields 267 are dominated by Rayleigh wave, which has a high sensitivity to S-wave veloc-268 ity. Meanwhile, P-wave velocity and Poisson's ratio are sensitive to the saturation 269 situation. We applied the K-mean cluster analysis algorithm in three data spaces 270  $(V_P, V_S, \nu)$ . As data pre-processings, we normalized the velocity and Poisson's 271 ratio to assign similar weights before the analysis. Specification of the number of 272 clusters is a critical step in the cluster analysis. Generally, the number of clusters 273

can be assigned according to the variance ration criterion (VRC) (Calinski and
Harabasz, 1974). Here, according to previous partitions for the GPR inversion
results and CPT results, we manually set a cluster number of three in this case
(Gueting et al., 2015).

The results of the cluster analysis are shown in Fig. 5. Although the veloc-278 ity and Poisson's ratio results in Fig. 2 both have an overall layered character, 279 however, the correlation between most structures is not clear. On the basis of the 280 corresponding cluster analysis considers with three data spaces, the spatial distri-281 bution of these homogeneous units is shown in Fig. 5. Cluster 1 is characterized 282 by higher P-wave velocity, higher Poisson's ratio, but with a lower S-wave ve-283 locity. Cluster 2 is characterized by lower P-wave velocity, lower Poisson's ratio, 284 but with a higher S-wave velocity. Cluster 3 is characterized by an intermediate 285 velocity and Poisson's ratio. Although the characterization of the subsurface has 286 been reduced to only three-parameter groups, the clustered section delineates the 287 major structural feature of the original models. 288

In order to validate our results of cluster analysis of seismic data, we compare 289 the seismic data clusters with the cluster analysis results of CPT data (Gueting 290 et al., 2015) in Fig. 5. The spatial distribution of the clusters shows a nice agree-291 ment, especially for the depth of 4-6 m. From the description of the grain size dis-292 tribution in borehole B32 by Gueting et al. (2015), the CPT cluster 1 corresponds 293 to in those depths where the grain size analysis shows gravel; CPT cluster 2 cor-294 responds to in those depths where the grain size analysis shows sand, and CPT 295 cluster 3 corresponds to in those depths where the grain size analysis shows an 296



(b) Cluster sections of two profile P1 (upper) and P2 (lower)

Figure 5: Cluster analysis. (a) The 3D plot of P-wave velocity, S-wave velocity, and Poisson's ratio. The red, blue and green dots are divided by the K-mean cluster analysis. The crosses delineate three cluster centres. (b) Cluster sections of the two profiles P1 and P2 according to the classification in (a). Numbers and colours refer to specific clusters.



Figure 6: Cluster comparison between the seismic results and CPT results. Cluster profile P2 according to the classify in Fig. 5(a). CPT clusters are referred to Gueting et al. (2015).

intermediate material such as gravelly sand or as sandy gravel. The water content
histograms, which is related to porosity also show that a relatively high porosity
for CPT cluster 2, relatively small porosity for CPT cluster 1, and an intermediate
porosity for CPT cluster 3, which are corresponded to the relative velocity and
Poisson's ratio's changes in seismic clusters.

#### 302 5. Conclusions

FWI of shallow seismic P- and Rayleigh waves proved to be a powerful tool for the reconstruction of viscoelastic multiparameter models of the shallow subsurface. Typically, the solution of the inverse problem is non-unique and, thus, there may be various solutions that differ in details but show equivalent overall fits to the data. We have explored the potential of applying the FWI method in a well-studied alluvial aquifer test site, which can offer secondary information to evaluate the reliability of the obtained inverted results. In addition, the benefit of
the parameters attenuation and mass density with information potential would be
studied in the future.

Cluster analysis of the multivariate seismic inversion results defined three dif-312 ferent facies in the aquifer cross-section. The classification of facies was con-313 firmed by the previous cluster analysis of CPT data. Moreover, the spatial distri-314 bution of facies in seismic data showed a nice agreement with the spatial distri-315 bution of CPT clusters. Comparison of the facies distribution with the previous 316 analysis showed that the derived lithological units correlate with the changes in 317 grain size and porosity. Overall, the experiment indicates that FWI of seismic 318 data can produce high-resolution results of the subsurface. Combined with cluster 319 analysis of the multivariate inverted data, FWI could give us an applicable ap-320 proach to classify geophysical facies. Integrating other geophysical and geotech-321 nical parameters (e.g. GPR data, grain size, and flowmeter data) can help to better 322 characterize the aquifer. 323

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